



INSTITUTE OF  
SPACE TECHNOLOGY & **SPACE APPLICATIONS**

der Bundeswehr

Universität  **München**

Session C3: Signals of Opportunity-Based Navigation Systems 1

## **LTE transmitter states estimation using a combined code and carrier phase observation model**

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# Overview - State of the Art with LTE/5G Positioning

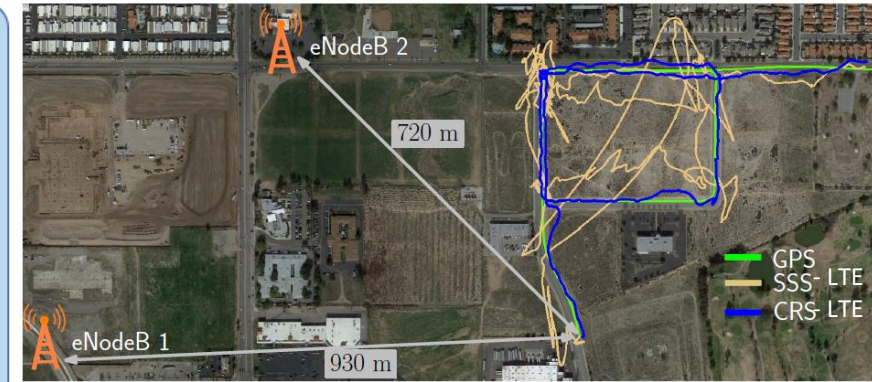
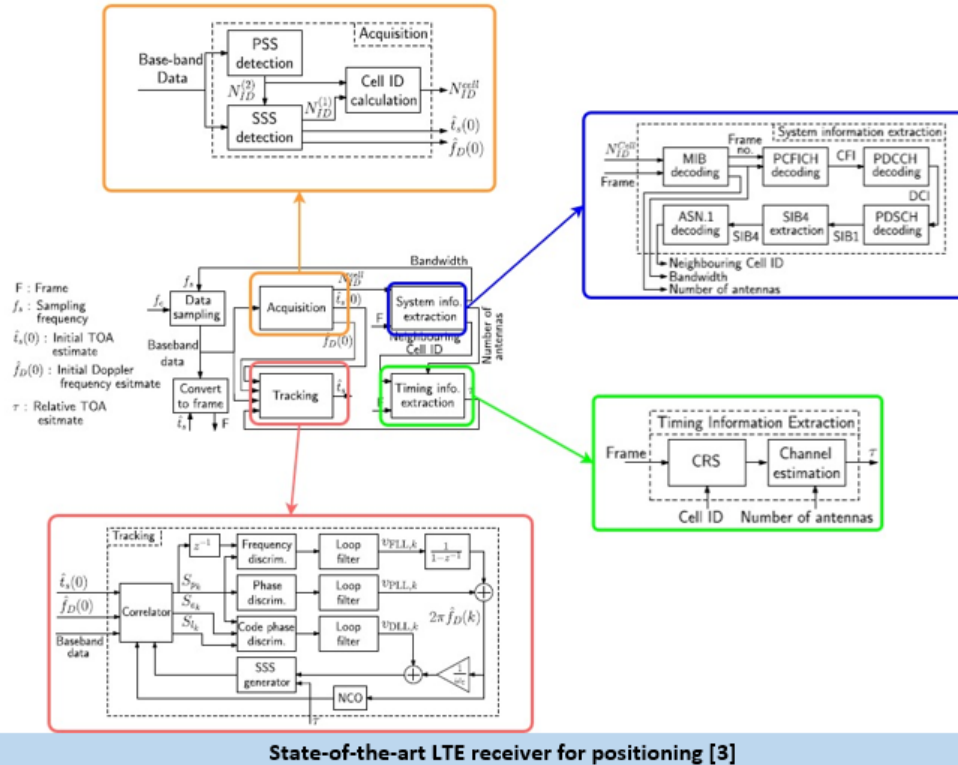
## Network based

- Standardized in LTE Release 9 with Positioning Reference Signal (PRS) [1]
- Dedicated resource allocation [2][3]:
  - Requires additional bandwidth => **constraint on provider**
  - Cellular provider specific => **not transmitted by all providers**
  - User position shared with network => **privacy compromised**

## UE Based

- Based on TOA estimation using synchronization dedicated signal resources e.g PSS, SSS and CRS.
- TOA estimation (advanced signal processing) techniques [4]:
  - First peak detection technique
  - Statistical modeling of CIR
  - Super-resolution algorithm
  - Delay-lock loop
- SOTA LTE receiver [3][5]:
  - Acquisition and tracking of LTE using PSS and SSS
  - Obtain first estimate of TOA using SSS
  - Update of TOA estimate based on CIR estimated using CRS

## LTE Positioning

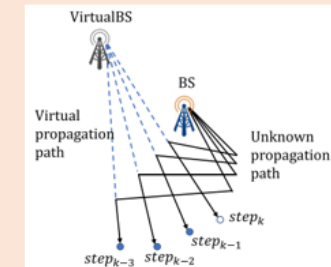


Vehicle-mounted receiver's GPS trajectory and trajectories estimated with LTE SSS and CRS signals [5]

## 5G Positioning

### Indoor Positioning

- Extension of TOA estimation for indoor environments.
- Mixed Line-Of-Sight (LOS) / Non-Line-Of-Sight (NLOS) environment.
- Reducing NLOS errors through [6]:
  - Smart selection of base station [7]
  - Virtual base station mapping for NLOS signals [8]
  - NLOS propagation model compensation [9]



Virtual base station concept [6]

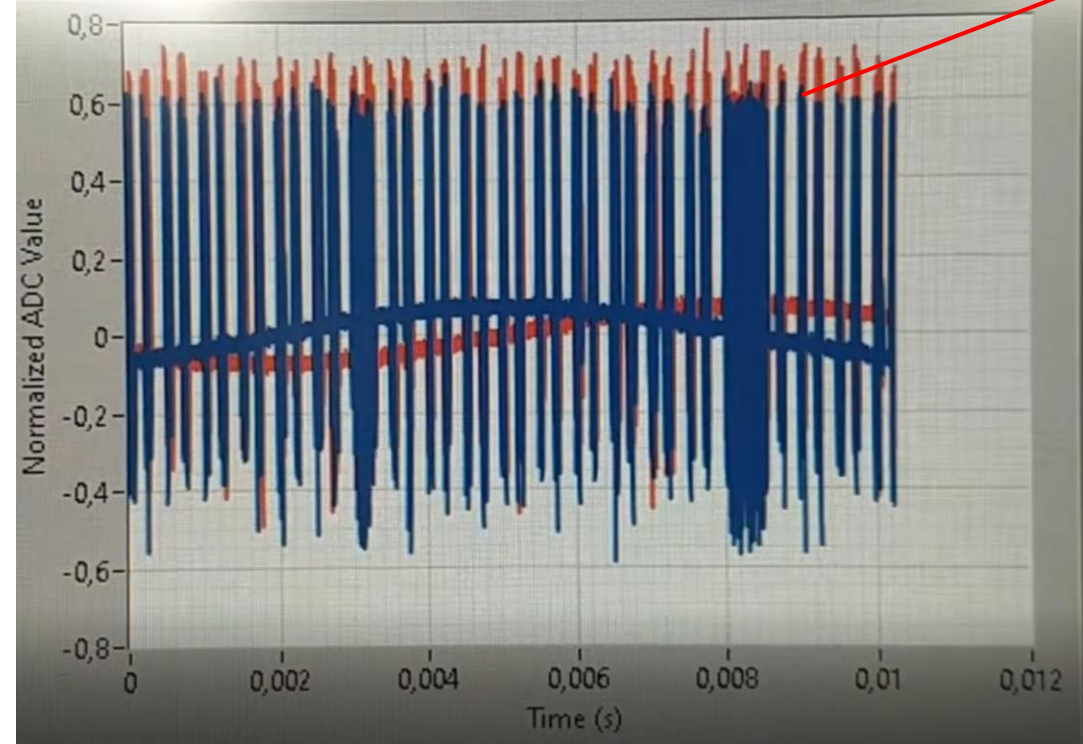
Urban canyon to indoor positioning evolution

# LTE signal introduction and MuSNAT implementation

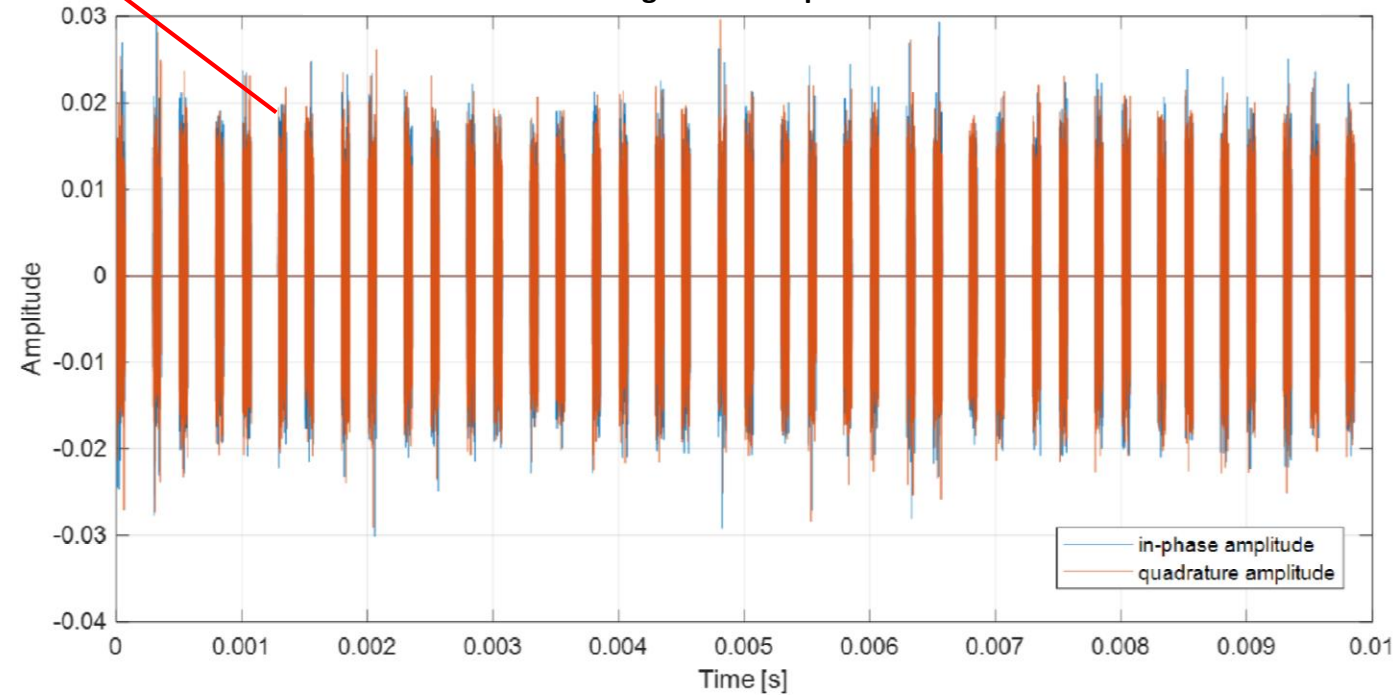
- **LTE tracking approach** -> generation of a single time-domain replica of the LTE SSS or CRS signal and using conventional GNSS-like DLL, PLL and FLL tracking.
- Code tracking achieved by cross-correlating measured signal with SSS/CRS code replica for complete LTE frame length (= 10 ms)

Each 'vertical' thin line represents an OFDM symbol of duration 66.6  $\mu$ s.

LTE frame within a measured signal transmitted from Amarisoft BS



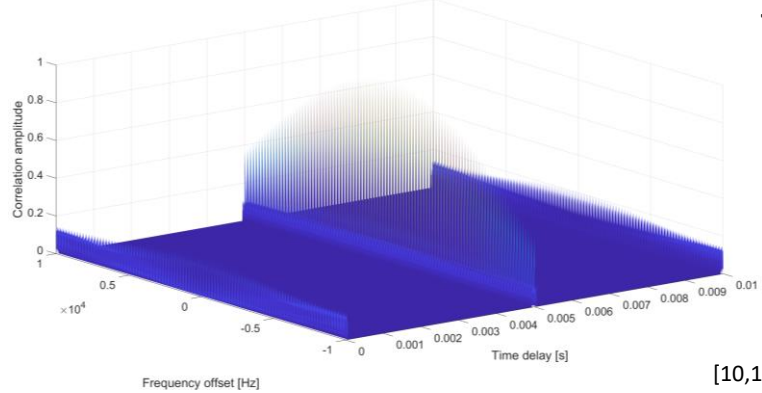
Time series of LTE CRS signal code replica for 10 subframes and 50 RBs



# SSS vs CRS signal comparison

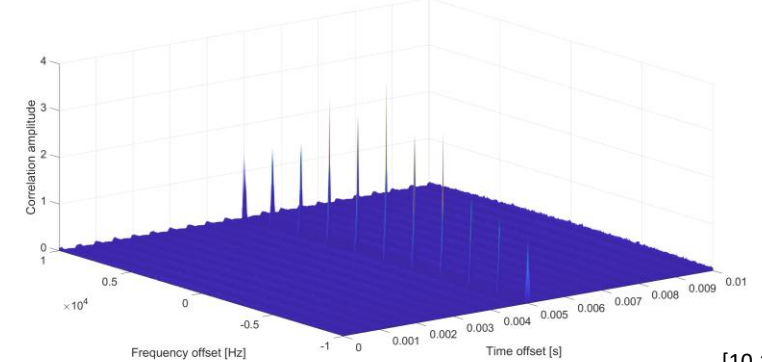
## SSS

3D autocorrelation function of the SSS sequence with a coherent integration of 10 ms



## CRS

3D correlation of the LTE CRS AP0 signal for 50 RB and a coherent integration time of 10 ms



### Transition from SSS based tracking to CRS based tracking



#### Pros:

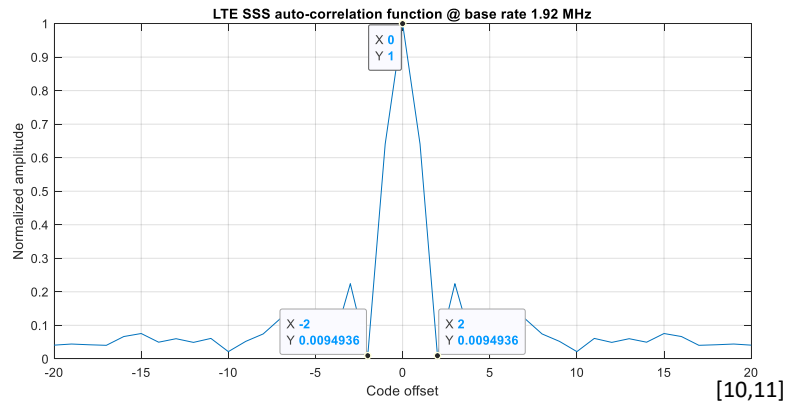
- Higher bandwidth → narrower correlation peak → low tracking jitter
- Less Doppler side-peaks

#### Cons:

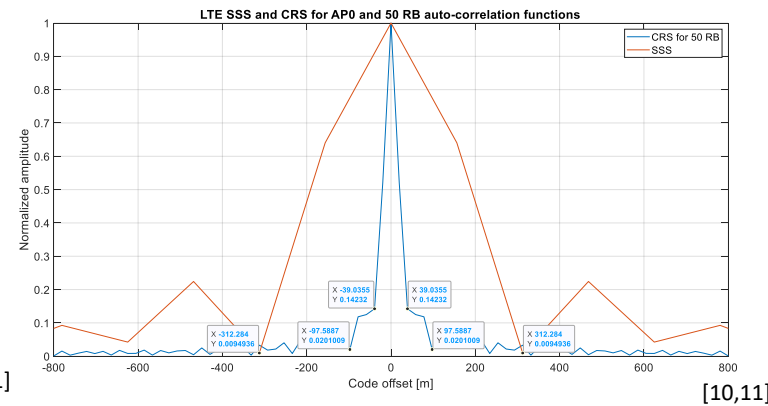
- More secondary peaks in code phase domain → solvable

[10,11] using BumpJump

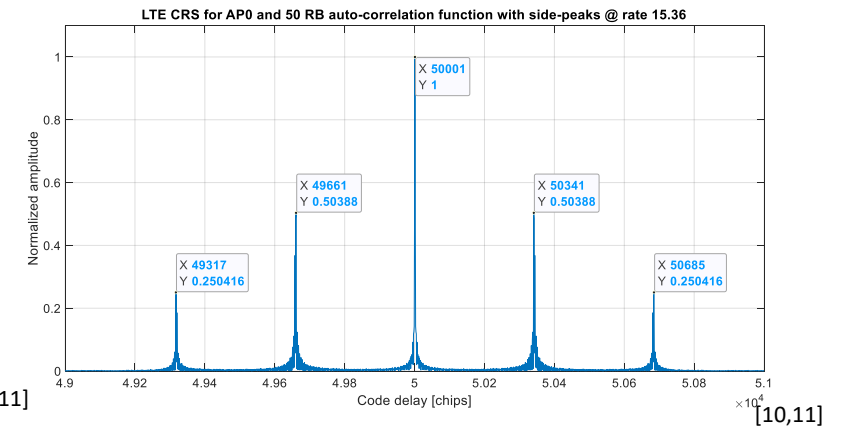
[10,11]



[10,11]



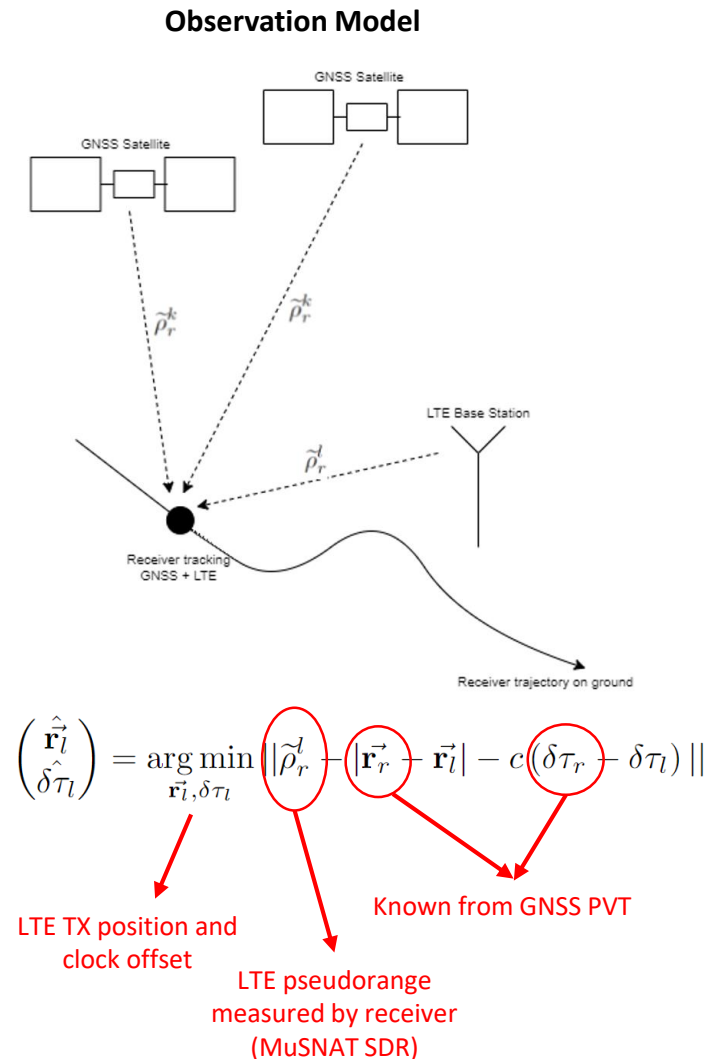
[10,11]



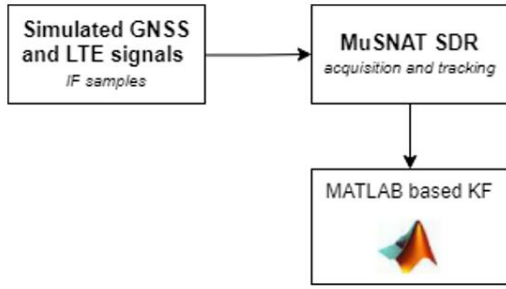
[10,11]

# LTE transmitter localization - Context

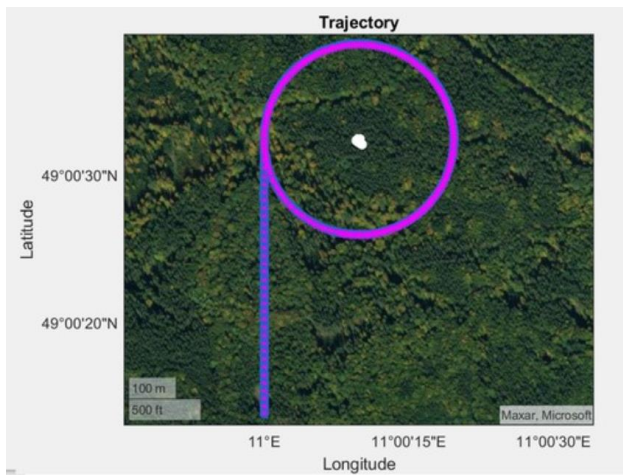
- Simultaneous Localization And Mapping (SLAM) using cellular signals as Signal Of Opportunity (SoP).
- Use of carrier phase of LTE has been previously investigated within:
  - **Differential navigation framework** with Base/Navigator for:
    - indoor environments [12]
    - UAV navigation [13]
  - **Absolute positioning framework** leveraging frequency stability of LTE base station clocks for UAV navigation [13]
- Experimental results published so far assume an **a-priori known transmitter position** obtained beforehand through a collaborative mapping [14] of the transmitter.
- With dynamic receivers or UAVs → estimation of transmitter states with carrier phase measurements can potentially be realized.
- The ‘knowledge’ of transmitter states can be broadcasted as part of pseudolite signals in future.



# Filter setup and simulation results



Processing chain for simulated signal



Ground track of simulated RX trajectory

Localization filter set-up → a six states Kalman Filter using code and carrier phase LTE measurements

$$\mathbf{x} = \begin{pmatrix} \vec{r}^l \\ N \\ \delta\tau^l \\ \delta\dot{\tau}^l \end{pmatrix} \quad (5) \quad \mathbf{y} = \begin{pmatrix} \rho_r^l \\ \phi_r^l \end{pmatrix}$$

$$\mathbf{B} = \text{diag}[\mathbf{I}_{4 \times 4}, \mathbf{B}_{clk}]^T$$

$$\mathbf{B}_{clk} = \begin{pmatrix} 1 & T \\ 0 & 1 \end{pmatrix}$$

$$\mathbf{H} = \begin{pmatrix} -(\vec{e}^l)^T & 0 & -c & 0 \\ -(\vec{e}^l)^T & \lambda & -c & 0 \end{pmatrix}$$

$$\mathbf{P}_0 = \text{diag}[\sigma_x^2, \sigma_y^2, \sigma_z^2, \sigma_N^2, \sigma_{\delta\tau}^2, \sigma_{\delta\dot{\tau}}^2]^T$$

$$\mathbf{R} = \text{diag}(\sigma_\rho^2, \sigma_\phi^2)$$

$$\mathbf{Q} = \text{diag}[\Omega_x^2, \Omega_y^2, \Omega_z^2, \Omega_N^2, \mathbf{Q}_{clk}]^T$$

$$\mathbf{Q}_{clk} = \begin{pmatrix} S_{\delta\tau_s} T + S_{\delta\dot{\tau}_s} \frac{T^3}{3} & S_{\delta\dot{\tau}_s} \frac{T^2}{2} \\ S_{\delta\dot{\tau}_s} \frac{T^2}{2} & S_{\delta\dot{\tau}_s} T \end{pmatrix}$$

Kalman Filter Time Update

$$\mathbf{x}_i^- = \mathbf{B}\mathbf{x}_{i-1}$$

$$\mathbf{P}_i^- = \mathbf{B}\mathbf{P}_{i-1}\mathbf{B}^T + \mathbf{Q}$$

Kalman Filter Measurement Update

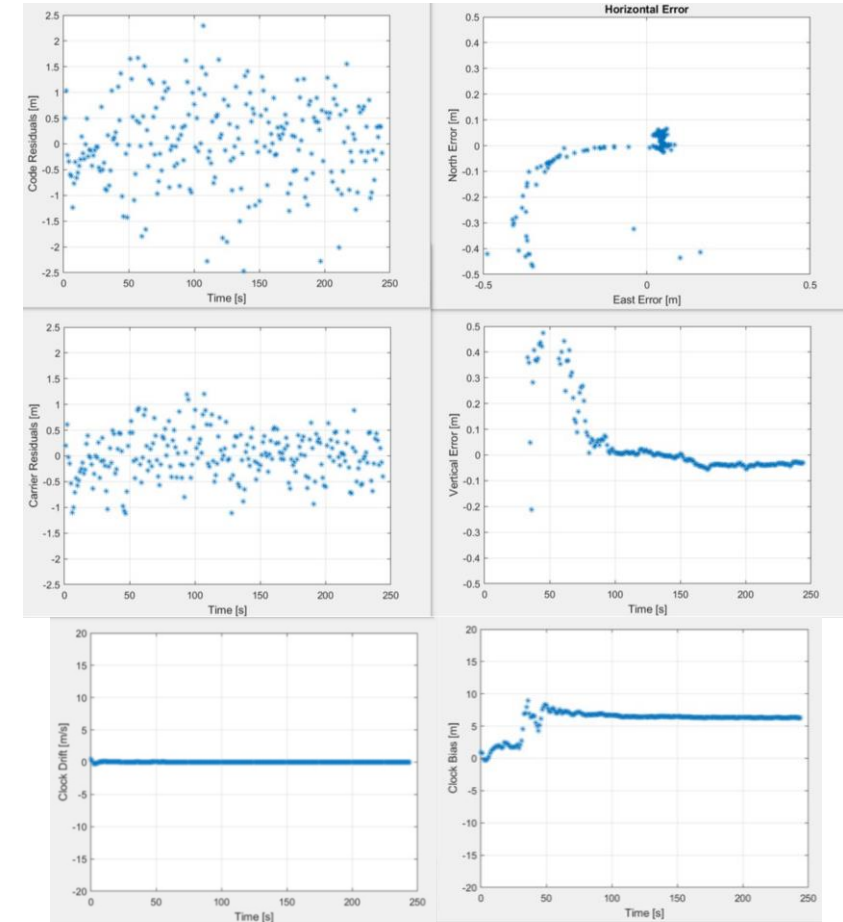
$$\mathbf{z}_i = \mathbf{y}_i - \mathbf{H}\mathbf{x}_i^-$$

$$\mathbf{K}_i = \mathbf{P}_i^- \mathbf{H}^T (\mathbf{H}\mathbf{P}_i^- \mathbf{H}^T + \mathbf{R})^{-1}$$

$$\mathbf{x}_i^+ = \mathbf{x}_i^- + \mathbf{K}_i \mathbf{z}_i$$

$$\mathbf{P}_i^+ = (\mathbf{I} - \mathbf{K}_i \mathbf{H}) \mathbf{P}_i^-$$

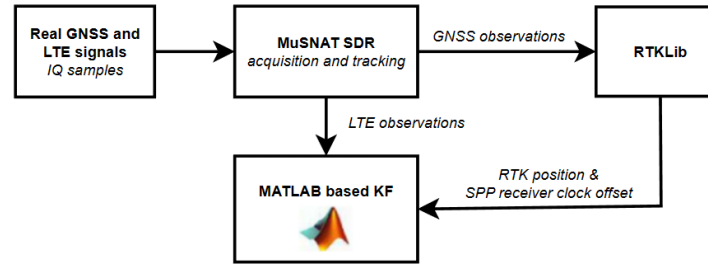
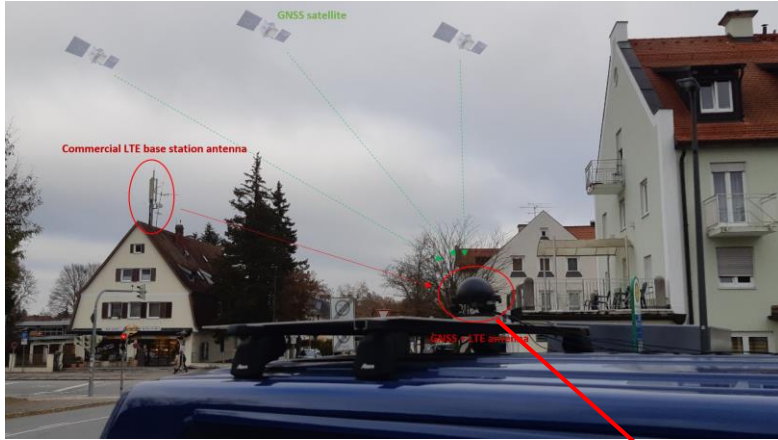
## Localization Filter Results



KF\_states = [PosX, PosY, PosZ, floatAmbi, clkBias, clkDrift]

Estimation of carrier phase float ambiguity allows to use carrier phase for LTE transmitter localization

# Experimental set-up for real-signals



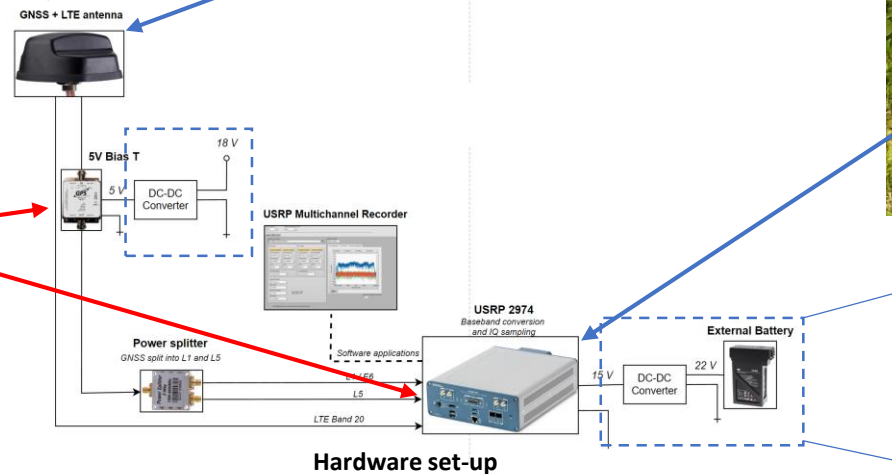
Processing chain for real signal



UAV - DJI Matrice 600 Pro drone



Ground vehicle – VW Transporter  
Measurement Bus



Hardware set-up

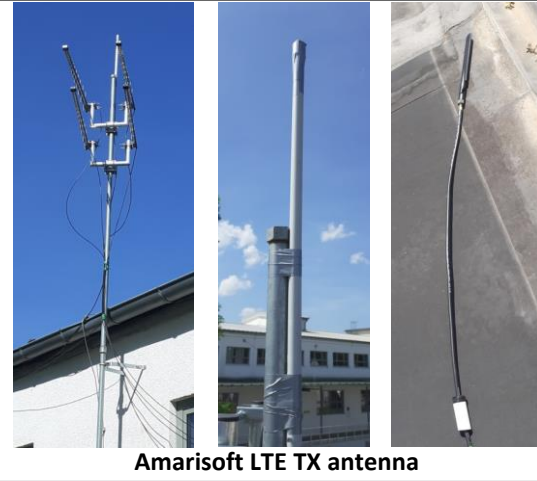
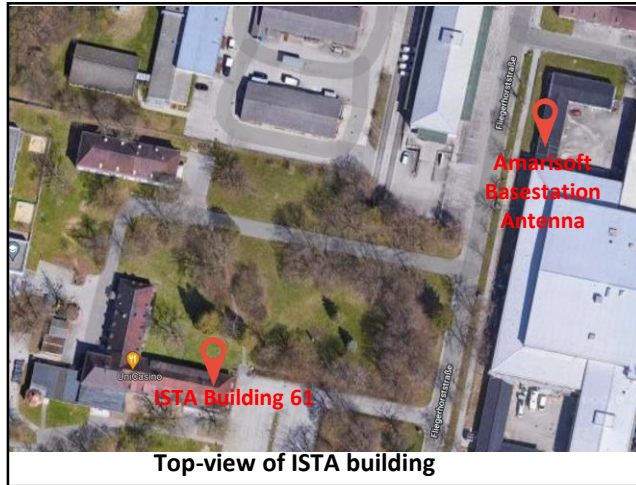
State	$I_L$ (A)	$V_e$ (V)	$P_L$ (W)
USRP OFF	0.06	14.98	0.94
USRP Stand-by	2.50	14.88	37.20
USRP ON Start-up	3.50	14.86	52.01
USRP Recording 3 streams @ 20 MHz	5.00	14.74	73.70
USRP Recording 4 streams @ 20 MHz	5.20	14.73	76.60
USRP Recording 4 streams @ 40 MHz	5.50	14.71	80.91
USRP Recording 4 streams @ 50 MHz	5.78	14.70	84.97

USRP 2974 tests with external battery



USRP 2974 IV-curve with DC-DC converter

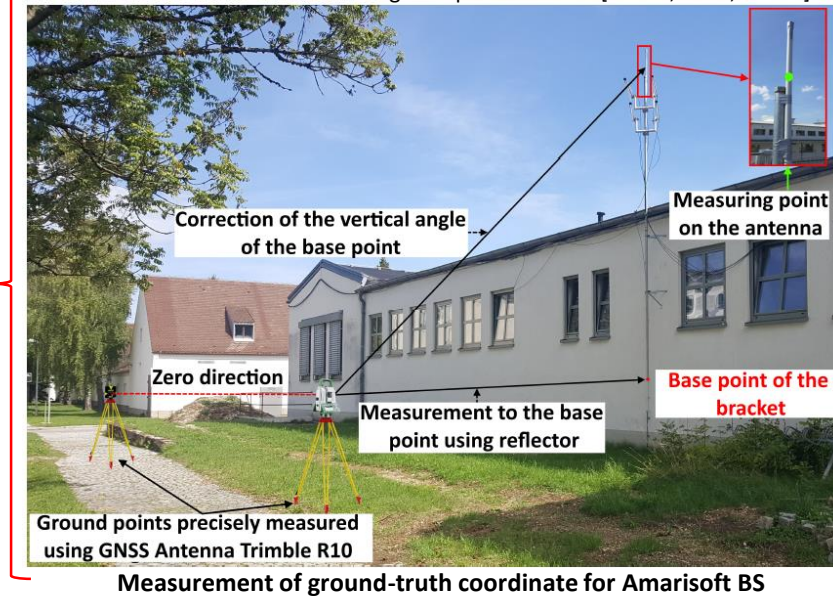
# Target base station – Amarisoft BS



Amarisoft BS

- Research oriented BS operated by institute ETTI within UniBW M campus
- PCI 1 at  $f_c = 2.665$  GHz
  - Omni-directional antenna
  - No inter-PCI clock bias or MIMO effects

\* PosDiff w.r.t Google Maps coordinate: [-29.71, -6.11, -33.78] m

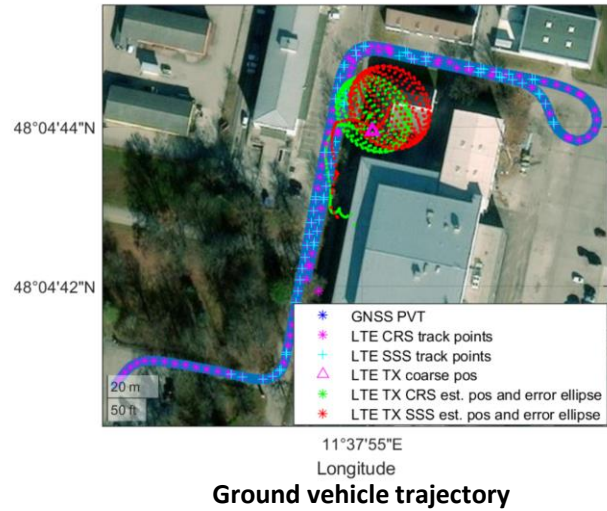


Ground-truth coordinate of Amarisoft BS TX antenna measured for reference using:

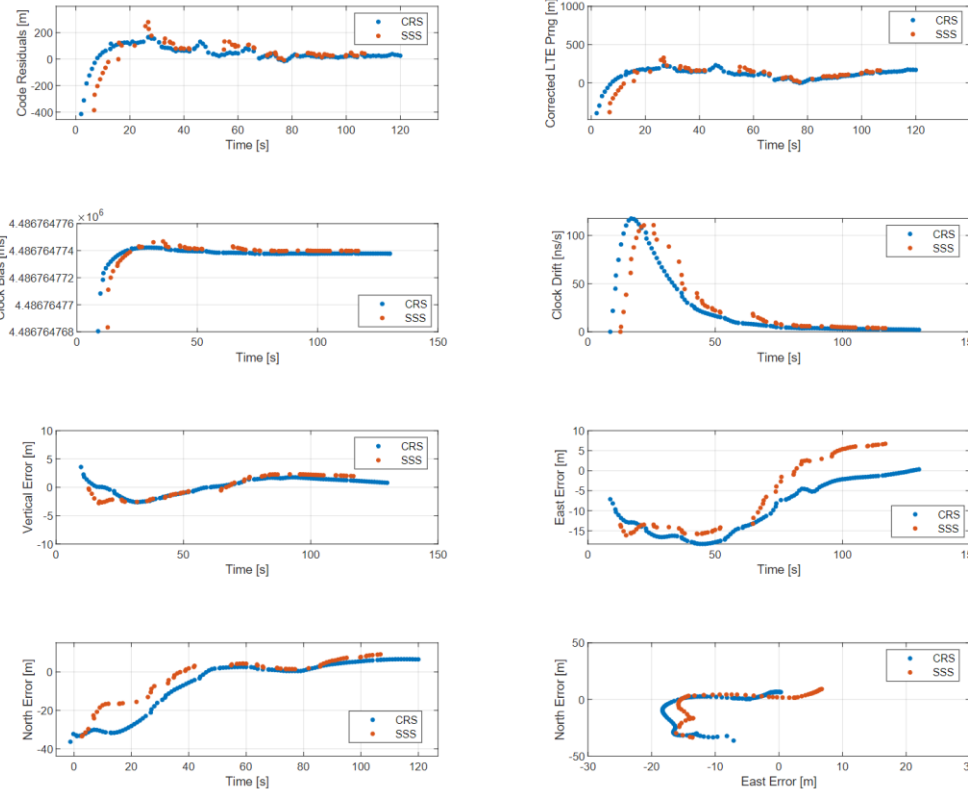
- Trimble R10 used for positioning of 02 static points
- Leica MS60 used for triangulation of antenna coordinates



# Ground vehicle with code-only measurements



## Localization filter results



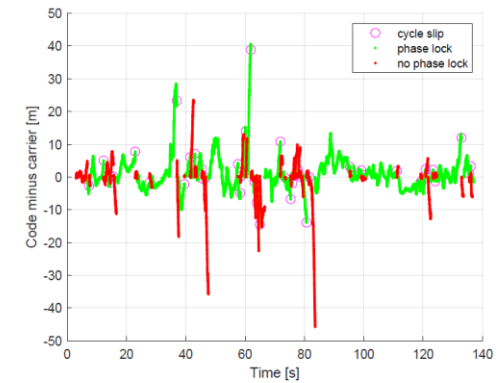
## Localization results using code-only measurements

State-variable	Symbol	Amarisoft BS	
		SSS	CRS
Pos. diff. X [m]*	$\delta x$	6.758	4.324
Pos. diff. Y [m]*	$\delta y$	-5.489	0.5632
Pos. diff. Z [m]*	$\delta z$	-7.606	-4.982
Absolute pos. diff. [m]*	$\Delta$	11.56	6.621
Clock Bias [ms]	$\delta \tau$	4.49e6	4.49e6
Clock Drift [ns/s]	$\delta \dot{\tau}$	3.736	2.089

\* Pos differences with respect to Google Map coordinates

CRS results are better than SSS results  
due to more stable signal tracking

## CMC Time series



(a) Amarisoft BS CRS tracking using Measurement Bus

CMC plot indicates  
several cycle-slips for  
Ground Vehicle

# UAV with code and carrier phase measurements

- For code + carrier measurements, 03 flights of UAV conducted near Amarisoft BS to sweep as much arc around the BS antenna as possible:

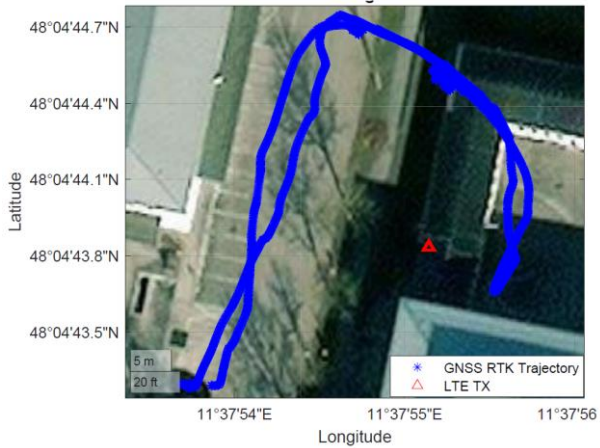


UAV flying near Amarisoft BS - photo

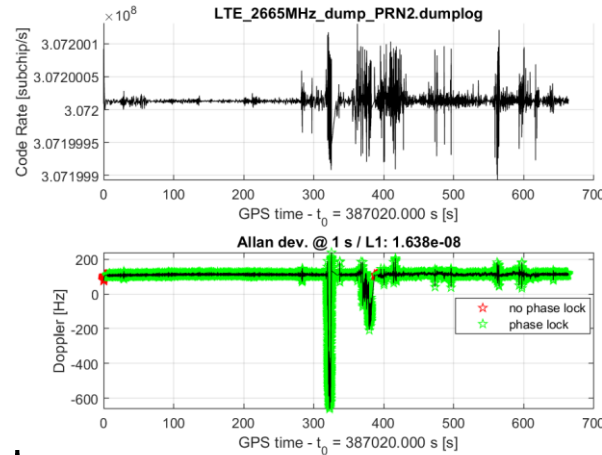


UAV flying near Amarisoft BS - video

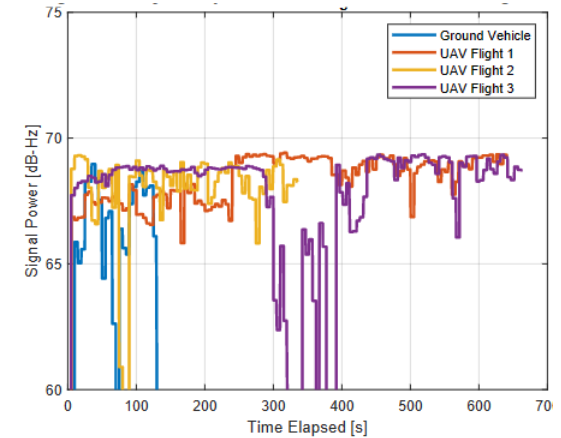
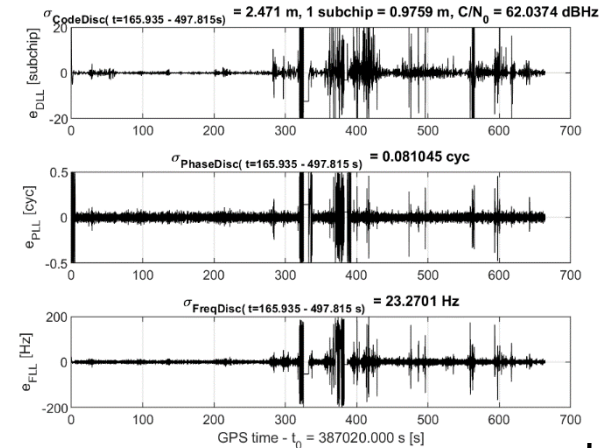
# Tracking results of UAV Flight 3



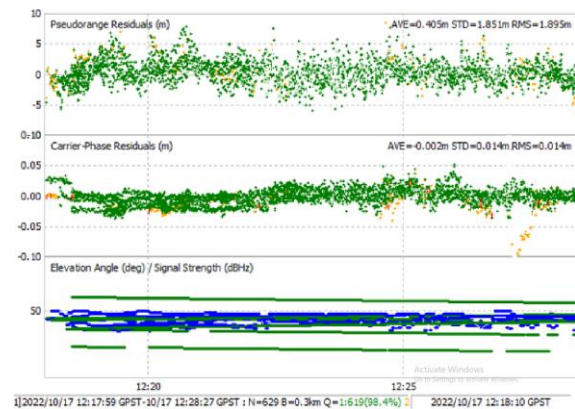
UAV flight trajectory



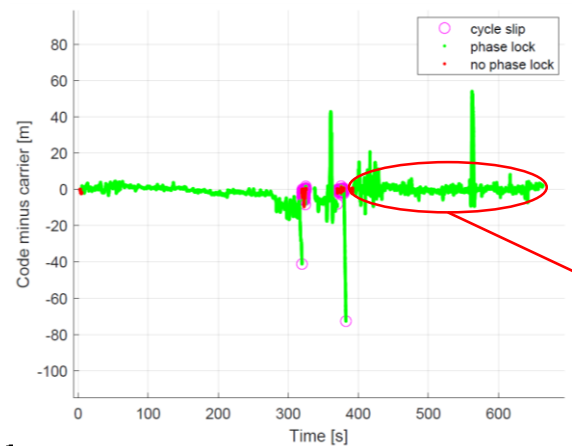
MuSNAT Tracking Results



Received signal power of all measurements



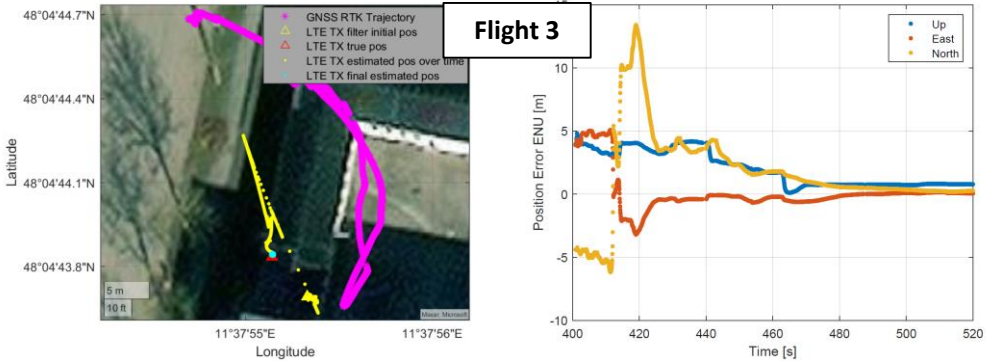
GNSS RTK results



Code-minus-carrier

Cycle-slip free pass with low CMC and dynamic receiver → chosen for further analysis with code + carrier phase measurements

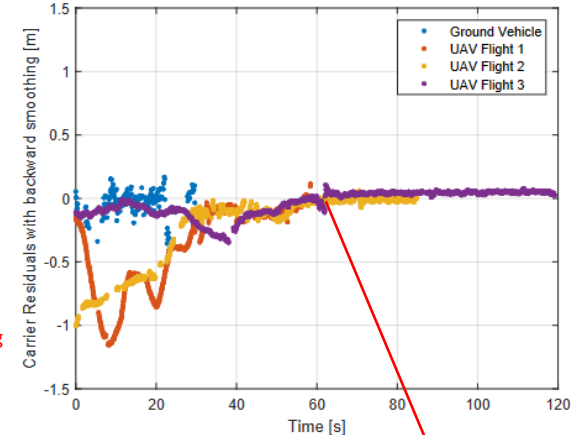
# Localization results of UAV Flight 3 with code and carrier phase measurements



Testcase	$\delta x$ [m]	$\delta y$ [m]	$\delta z$ [m]	$\text{norm}[\delta x, \delta y, \delta z]$ [m]
Ground Vehicle	0.464	0.010	-2.28	2.33
UAV Flight 1	0.590	0.226	-1.98	2.08
UAV Flight 2	0.686	1.29	-0.405	1.52
UAV Flight 3	-0.301	-0.117	-0.770	0.834

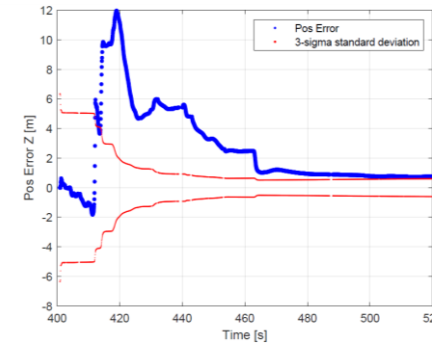
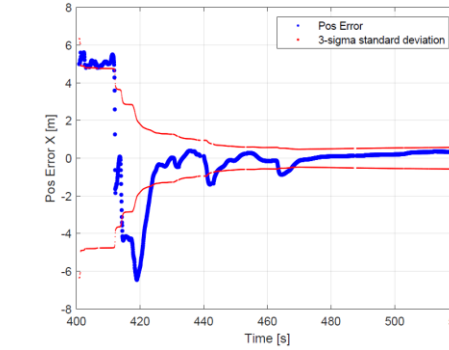
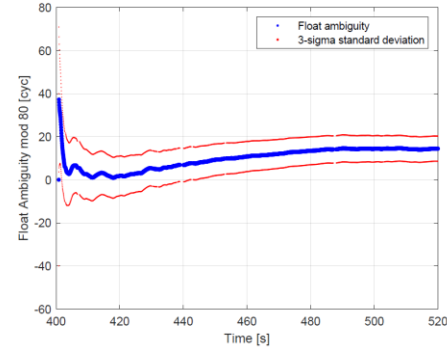
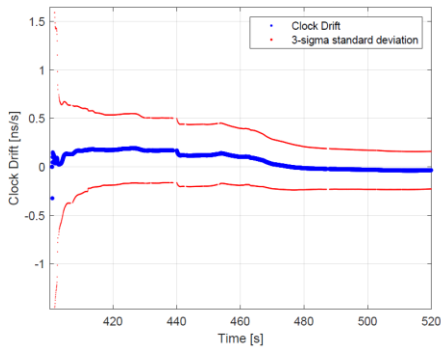
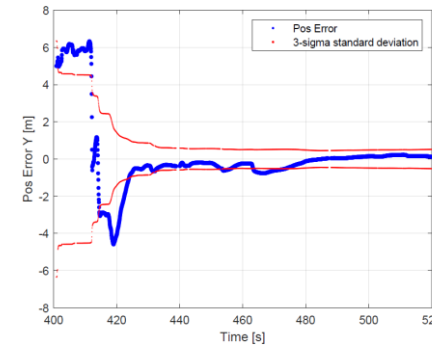
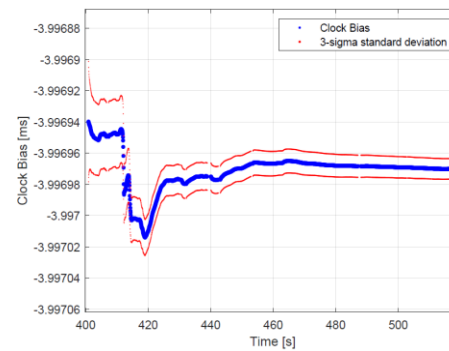
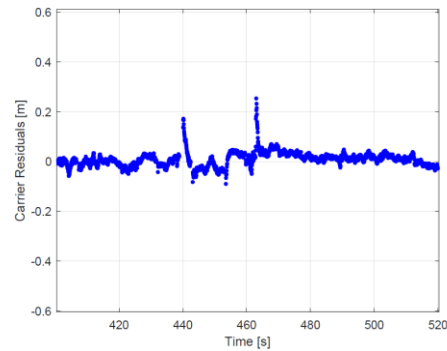
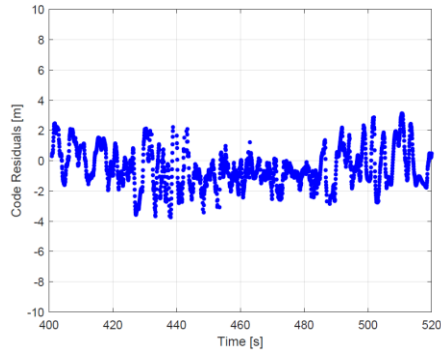
Localization filter results

Best results achieved with UAV Flight 3 having longest stable carrier-tracking pass duration



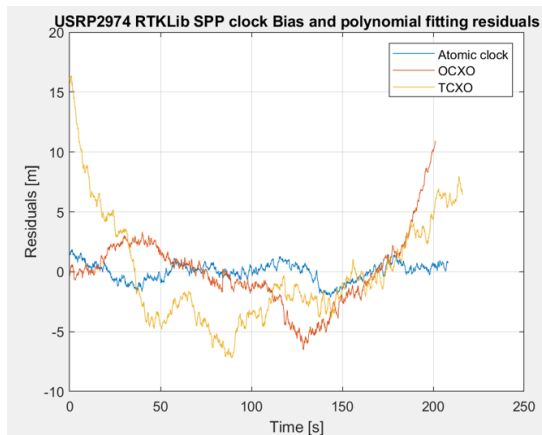
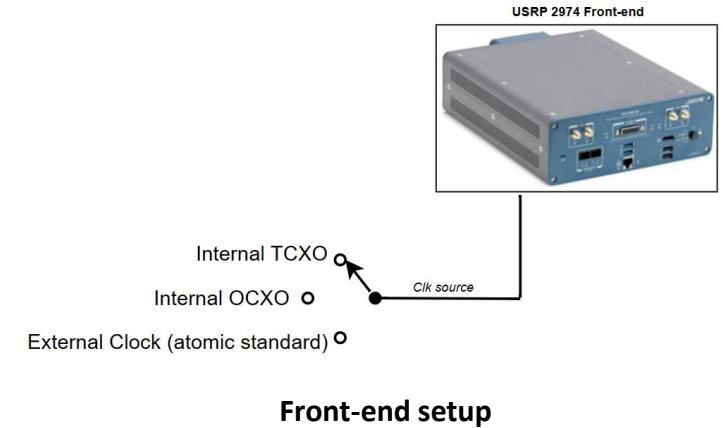
Convergence of carrier phase residuals after backward smoothing

Filter convergence time ~ 60 secs

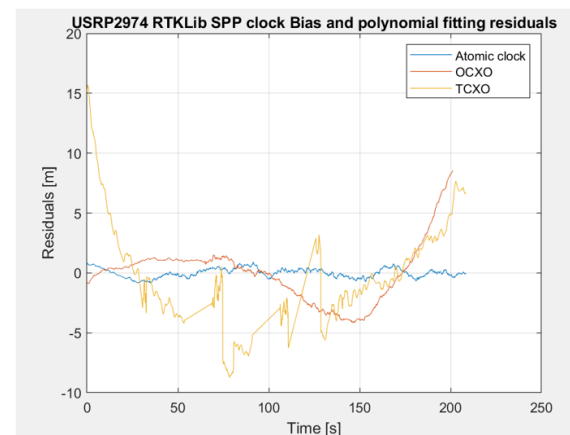


# Error sources -> GNSS SPP receiver clock error

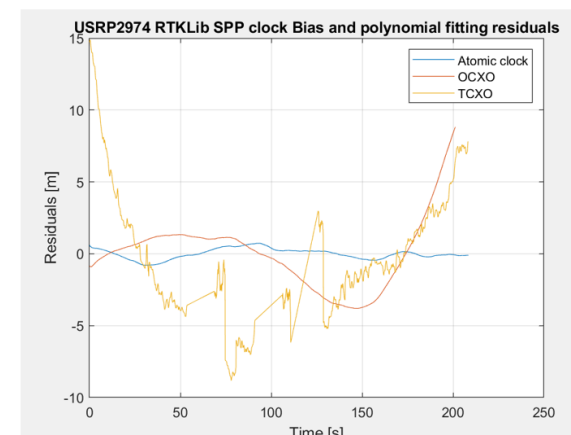
- Receiver clock offset gets eliminated in RTK
- For localization → filtered GNSS SPP clock error was used.
- 1<sup>st</sup> order polynomial fitted on measured receiver clock error
- Alternatively, a more stable on-board clock can be used.



RTKLib SPP clock offset residuals w.r.t 1-order poly



RTKLib PPP clock offset residuals w.r.t 1-order poly



RTKLib PPP clock offset residuals (with CarriersSmoothing ON) w.r.t 1 order poly

Residuals of measured receiver clock error w.r.t 1-order polynomial for a static receiver measurement

# Conclusions

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- LTE signal tracking can be realized in a GNSS oriented tracking architecture.
- CRS provides a better tracking performance with high  $C/N_0$  than SSS due to narrower correlation function and more distant Doppler side-peaks.
- Amarisoft Base station serves as a good platform for verifying calibration procedure due to easy access and availability of ground truth.
- It is possible to use carrier phase tracking of LTE signal for the purpose of transmitter localization given an accurate information of the receiver states
- Efficient cycle-slip detection scheme should be employed.
- With combined code and carrier-phase observations, a position accuracy of within 0.3 m is achieved in North and Up directions and within 1 m in the Up direction for at least one UAV flight.
- One of the biggest error sources is the SPP receiver clock offset.

# Way forward



Transmitter setup

02 LTE transmitters:  
Each with a different PCI  
and line-of-sight position

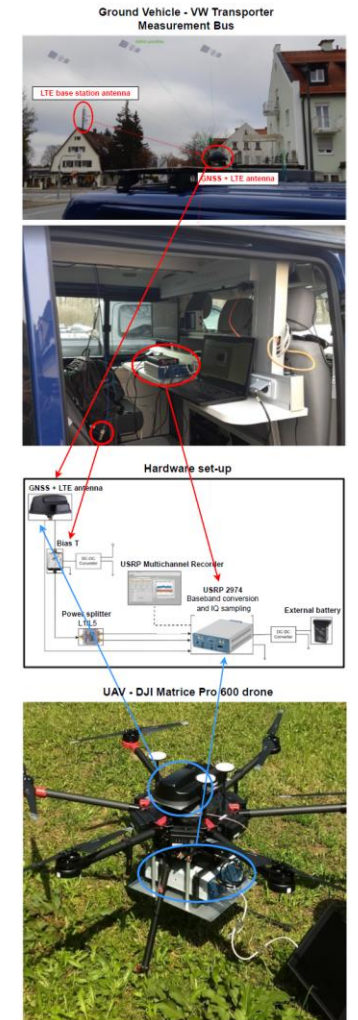


Receiver setup

03 receivers:  
- Static (base)  
- Ground Vehicle (rover)  
- UAV with on-board  
atomic clock (rover)

## Testcases planned for future:

- Computation of LTE DD observations using two LTE transmitters and two receivers
- Evaluation of code and carrier phase noise of LTE CRS as function of carrier-to-noise ratio
- Comparison of code and carrier phase noise for Ground Vehicle and UAV receiver platforms
- Localization of LTE transmitter through a UAV receiver platform with on-board atomic clock
- Precise localization of LTE transmitter using LTE DD observations
- Differential positioning of a Ground Vehicle with GNSS and one LTE signal using a-priori known LTE transmitter position



03 receivers -> Ground Vehicle, UAV and static base

# References

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- [12] Abdallah, Ali A., Shamaei, Kimia, Kassas, Zak M., "Indoor Positioning Based on LTE Carrier Phase Measurements and an Inertial Measurement Unit," Proceedings of the 31st International Technical Meeting of the Satellite Division of The Institute of Navigation (ION GNSS+ 2018), Miami, Florida, September 2018, pp. 3374-3384.
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